

**ENGR 292 Fluids and Thermodynamics**

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**Pump and Pipe Example**

**Design a Pump and Pipe System for the starter problem of Technologist**

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**Step 1**

**Rough Layout**

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**Step 1 (cont'd)**

**Rough Layout**

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**Step 2**

**Pipe Size (Discharge):**

- $Q = vA \rightarrow A = \frac{Q}{v}$
- $A = \frac{\pi D^2}{4} \rightarrow D = \sqrt{\frac{4A}{\pi}}$
- $v$  : **Recommended Velocity**
  - We choose  $v = 3\text{ m/s}$  (Design)
  - So  $A = \frac{Q}{v} = \frac{0.006\text{ m}^3/\text{s}}{3\text{ m/s}} = 0.002\text{ m}^2$
- $\therefore D = \sqrt{\frac{4A}{\pi}} = \sqrt{\frac{(4)(0.002)}{\pi}} \approx 0.050463\text{ m} = 50.463\text{ mm}$

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**Step 2 (cont'd)**

**Pipe Size:**

- Choose a close real size
- [http://www.engineeringtoolbox.com/asm-e-steel-pipes-sizes-d\\_42.html](http://www.engineeringtoolbox.com/asm-e-steel-pipes-sizes-d_42.html)
- SCH 40 ... ID=52.501mm
- That is for 2" SCH 40 Pipe
- $D_{\text{Discharge}} = 52.501 \times 10^{-2}\text{ m}$
- $A_{\text{Discharge}} = 21.648 \times 10^{-4}\text{ m}^2$

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### Step 3

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**Suction Line Size:**

- One standard size larger than the discharge
- Choose 2 1/2" SCH 40
- ID=62.713mm
- $D_{Suction} = 62.713 \times 10^{-2}m$
- $A_{Suction} = 30.889 \times 10^{-4}m^2$

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### Step 4

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**Calculate Actual Flow Velocity of Discharge**

$$v_{Discharge} = \frac{Q}{A_{Discharge}} = \frac{0.006m^3/s}{21.648 \times 10^{-4}m^2}$$

$$= 2.77 \text{ m/s}$$

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### Step 4 (cont'd)

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**Calculate Actual Flow Velocity of Suction**

$$v_{Suction} = \frac{Q}{A_{Suction}} = \frac{0.006m^3/s}{30.889 \times 10^{-4}m^2}$$

$$= 1.94 \text{ m/s}$$

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### Step 5

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**Determine the Reynolds Number**

$$N_R = \frac{vD\rho}{\mu}$$

at 5°C ...

$$\rho = 999.9 \text{ kg/m}^3$$

$$\mu = 1.519 \times 10^{-4} \text{ kg/(ms)}$$

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### Step 5 (cont'd)

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**Reynolds Number (Discharge)**

$$N_{R\_Discharge} = \frac{v_{Discharge} D_{Discharge} \rho}{\mu}$$

$$= \frac{(2.77)(52.501 \times 10^{-3})(999.9)}{1.519 \times 10^{-4}} = 9.6 \times 10^4$$

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### Step 5 (cont'd)

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**Reynolds Number (Suction)**

$$N_{R\_Suction} = \frac{v_{Suction} D_{Suction} \rho}{\mu}$$

$$= \frac{(1.94)(62.713 \times 10^{-3})(999.9)}{1.519 \times 10^{-4}} = 8.0 \times 10^4$$

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### Step 6

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**Pipe Material: Commercial Steel**

<http://www.pipeflow.com/sitemap/pipe-roughness>

**Roughness:**

$$\varepsilon = 0.0045 \text{ (mm)}$$

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### Step 7

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**Relative Roughness:**

**Discharge Pipe:**

$$\frac{\varepsilon}{D_{\text{Discharge}}} = \frac{0.0045}{52.501} = 0.00086$$

**Suction Pipe:**

$$\frac{\varepsilon}{D_{\text{Suction}}} = \frac{0.0045}{62.713} = 0.00072$$

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### Step 7

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**Relative Roughness:**

**Discharge Pipe:**

$$\frac{D_{\text{Discharge}}}{\varepsilon} = \frac{52.501}{0.0045} = 11666.89$$

**Suction Pipe:**

$$\frac{D_{\text{Suction}}}{\varepsilon} = \frac{62.713}{0.0045} = 13936.22$$

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### Step 8

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**Friction Factor:**

**From Moody Diagram**

$$f_{\text{Discharge}} = f_{\text{Suction}} \approx 0.0217$$

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### Step 9

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**Pipe Length:**

$$L_{\text{Discharge}} = 9 + 1 + 1 + 5 = 16 \text{ (m)}$$

$$L_{\text{Suction}} = 1 + 1 + 2 = 4 \text{ (m)}$$

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### Step 10

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**Pipe Friction Head Loss:**

$$h_L = f \frac{L v^2}{D 2g}$$

$$h_{L, \text{Discharge}} = (0.0217) \frac{16 (2.77)^2}{52.501 \times 10^{-3} 2(9.81)} = 2.59 \text{ (m)}$$

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### Step 10 (cont'd)

#### Pipe Friction Head Loss:

$$h_L = f \frac{L}{D} \frac{v^2}{2g}$$

$$h_{L_{Suction}} = (0.0217) \frac{4}{62.713 \times 10^{-3}} \frac{(1.94)^2}{2(9.81)}$$

$$= 0.266 \text{ (m)}$$

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### Step 11

#### Fitting Head Loss: Minor Losses:

$$h_L = \left[ \sum K \right] \frac{v^2}{2g}$$

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### Step 11 (cont'd)

#### Fitting Head Loss: Minor Losses

##### Discharge:

- 2 gate valves:  $K = 0.16$  each
- 3 elbows:  $K = 0.39$  each
- Discharge:  $K = 1.0$

$$h_{i_{Discharge}} = [(0.16) \times 2 + (0.39) \times 3 + (1.0) + 0] \frac{1.94^2}{2 \times 9.81}$$

$$= 0.974 \text{ (m)}$$

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### Step 11 (cont'd)

#### Fitting Head Loss: Minor Losses

##### Suction:

- 1 check valve:  $K = 2.0$  each
- 1 elbow:  $K = 0.39$  each

$$h_{L_{Suction}} = [(2.0) + (0.39)] \frac{1.94^2}{2 \times 9.81}$$

$$= 0.458 \text{ (m)}$$

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### Step 12

#### Determine the pump head:

##### Reorder the general energy equation:

$$\frac{p_1}{\gamma} + z_1 + \frac{v_1^2}{2g} + h_A - h_R - h_L = \frac{p_2}{\gamma} + z_2 + \frac{v_2^2}{2g}$$

To:

$$h_A = \frac{p_2 - p_1}{\gamma} + z_2 - z_1 + \frac{v_2^2 - v_1^2}{2g} + h_R + h_L$$

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### Step 12 (cont'd)

#### Determine the pump head:

$$p_1 = \rho gh = (999.9)(9.81)(1) = 9.81 \text{ kpa (gage)}$$

$$p_2 = 0 \text{ kpa (gage)}$$

$$\gamma = \rho g = 999.9 \times 9.81 = 9.81 \text{ kN/m}^3$$

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### Step 12 (cont'd)

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**Determine the pump head:**

**So**

$$h_A = \frac{p_2 - p_1}{\gamma} + z_2 - z_1 + \frac{v_2^2 - v_1^2}{2g} + h_R + h_L$$

$$= \frac{0 - 9.81}{9.81} + [(1 + 1 + 9) - 0] + \frac{2.77^2 - 1.94^2}{2 \times 9.81} + 0$$

$$+ [0.266 + 0.458 + 2.59 + 0.974] = 14.49 \text{ (m)}$$

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### Step 13

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**Pump Selection – Pump Curves**

$$Q = 95.1 \text{ (US GPM)}$$

$$h_A = 14.49 \text{ (m)} = 47.54 \text{ (ft)}$$

After a little searching ...

*B&G Model 1510 – 2E at 1150 PRM can be an option*

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### Step 14

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**Check Suction Design:**

$$NPSH_A > NPSH_R$$

**Or Change Design !**

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