



Given: A heat exchanger with a $\frac{1}{2}$ " copper central pipe and a $1\frac{1}{2}$ " sched 40 outer pipe. Inner is cold water, outer is hot water.

Type K copper $\frac{1}{2}$ "

$$OD = 0.01588 \text{ m}$$

$$ID = 0.01339 \text{ m}$$

$$A = 1.407 \times 10^{-4} \text{ m}^2$$

Sched 40 $1\frac{1}{2}$ "

$$OD = 0.0483 \text{ m}$$

$$ID = 0.0409 \text{ m}$$

$$A = 1.314 \times 10^{-3} \text{ m}^2$$

$$T_{C,in} = 5^\circ\text{C}, \quad T_{C,out} = 60^\circ\text{C}, \quad T_{H,in} = 90^\circ\text{C} \leftarrow \text{From rooftop heater}$$

$$U = 1250 \text{ W/m}^2\cdot\text{K}, \quad Q_H = 110 \text{ W/min} = 0.001833 \text{ m}^3/\text{s}, \quad \dot{m}_H = (0.001833 \text{ m}^3/\text{s})(990 \text{ kg/m}^3) = 1.815 \text{ kg/s}$$

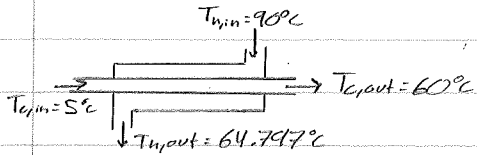
Five shower heads each requiring 10 L/min

$$Q_C = (5)(10 \text{ L/min}) = 50 \text{ L/min} = 0.000833 \text{ m}^3/\text{s}, \quad \dot{m}_C = (0.000833 \text{ m}^3/\text{s})(996 \text{ kg/m}^3) = 0.83 \text{ kg/s}$$

Counter Flow

$$Q_c = \dot{m} C_p (T_{out} - T_{in}) = (0.83 \text{ kg/s})(4.3)(60 - 5) = \boxed{196.295 \text{ kW}}$$

$$Q_H = \dot{m} C_p (T_{out} - T_{in}) \rightarrow T_{out} = T_{in} - \frac{Q}{\dot{m} C_p} = 90^\circ\text{C} - \frac{196.295 \text{ kW}}{(1.815 \text{ kg/s})(4.3)} = \boxed{64.797^\circ\text{C}}$$



$$\Delta T_1 = T_{h,in} - T_{c,out} = 90 - 60 = 30^\circ\text{C}$$

$$\Delta T_2 = T_{h,out} - T_{c,in} = 64.797 - 5 = 59.797^\circ\text{C}$$

$$\Delta T_{LM} = \frac{\Delta T_1 - \Delta T_2}{\ln(\Delta T_1 / \Delta T_2)} = \frac{30 - 59.797}{\ln(30 / 59.797)} = \boxed{43.1993^\circ\text{C}}$$

$$Q = U A_s \Delta T_{LM} \rightarrow A_s = \frac{Q}{U \Delta T_{LM}} = \frac{196295}{(1250)(43.1993)} = 3.635 \text{ m}^2 = \boxed{39.13 \text{ ft}^2}$$

$$A_s = \pi D L \rightarrow L = \frac{A_s}{\pi D} = \frac{3.635 \text{ m}^2}{\pi(0.01588)} = \boxed{72.8656 \text{ m}}$$

$$C_h = \dot{m}_h C_{p,h} = (1.815 \text{ kg/s})(4.3) = 7.805 \text{ kW/}^\circ\text{C}$$

$$C_c = \dot{m}_c C_{p,c} = (0.83 \text{ kg/s})(4.2) = 3.486 \text{ kW/}^\circ\text{C}$$

$$C_{min} = C_c = 3.486 \text{ kW/}^\circ\text{C}$$

$$C = \frac{C_{min}}{C_{max}} = \frac{3.486}{7.805} = 0.4467$$

$$NTU = \frac{U A}{C_{min}} = \frac{(1250)(3.635)}{3.486 \times 10^3} = \boxed{1.3034}$$

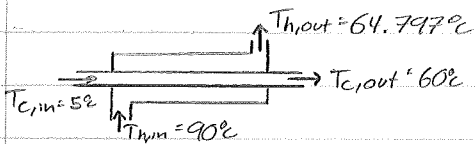
From Fig 16-26 (b)

$$\epsilon = \boxed{65\%}$$

Not Practical!

NTU is less than 3 \therefore Good design!

Parallel Flow



$$\Delta T_1 = T_{H,in} - T_{C,in} = 90 - 5 = 85^\circ\text{C}$$

$$\Delta T_2 = T_{H,out} - T_{C,out} = 64.797 - 60 = 4.797^\circ\text{C}$$

$$\Delta T_{LM} = \frac{\Delta T_1 - \Delta T_2}{\ln(\Delta T_1 / \Delta T_2)} = \frac{85 - 4.797}{\ln(85 / 4.797)} = \boxed{27.9003^\circ\text{C}} \quad \checkmark$$

$$Q = UA_s \Delta T_{LM} \rightarrow A_s = \frac{Q}{U \Delta T_{LM}} = \frac{196295}{(1250)(27.9003)} = \boxed{5.6285 \text{ m}^2} = 60.58 \text{ ft}^2 \quad \checkmark$$

$$A_s = \pi D L \rightarrow L = \frac{A_s}{\pi D} = \frac{5.6285 \text{ m}^2}{\pi(0.01522)} = \boxed{117.821 \text{ m}} \quad \checkmark$$

$$NTU = \frac{UA}{C_{min}} = \frac{(1250)(5.6285)}{3.486 \times 10^3} = \boxed{2.0182} \quad \checkmark$$

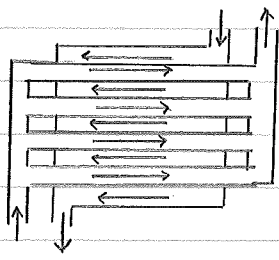
From Fig 16-26(a)

$$\epsilon = \boxed{67\%} \quad \checkmark$$

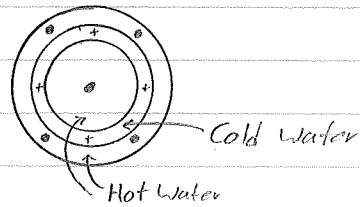
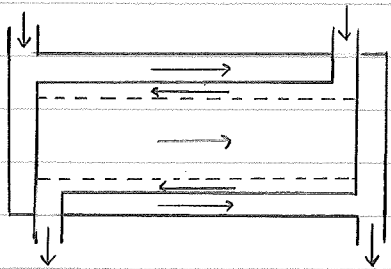
Not Practical!

NTU is less than 3 \therefore Good design! \checkmark

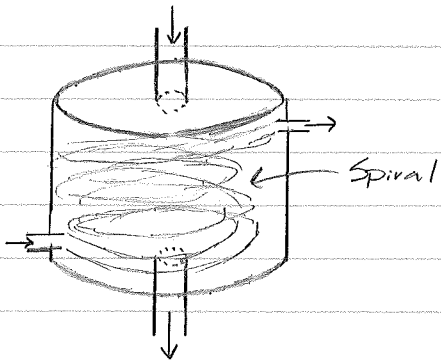
Alternate Designs



Cold flows through multiple tubes in a Hot bath.



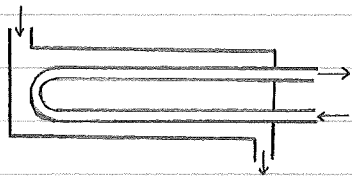
Hot flows around both sides of cold pipe.



Cold flows through upward spiral in a hot bath.

GOOD

U-Tube (1 shell pass, 2 tube pass, counter flow)



Start with data for counter flow

$$\Delta T_{LM} = \boxed{43.1993^\circ\text{C}}$$

$$t_1 = 5^\circ\text{C}$$

$$t_2 = 60^\circ\text{C}$$

$$T_1 = 90^\circ\text{C}$$

$$T_2 = 64.797^\circ\text{C}$$

$$P = \frac{t_2 - t_1}{T_1 - t_1} = \frac{60 - 5}{90 - 5} = 0.647$$

$$P = \frac{T_1 - T_2}{t_2 - t_1} = \frac{90 - 64.797}{60 - 5} = 0.458$$

From Figure 16-18 (a)

$$F = 0.85$$

$$\Delta T_{LM} = F \Delta T_{LM,cf} = (0.85)(43.1993) = \boxed{36.7194^\circ\text{C}}$$

$$Q = UA_s \Delta T_{LM} \Rightarrow A = \frac{Q}{U \Delta T_{LM}} = \frac{196295}{(1250)(36.7194)} = 4.27665 \text{ m}^2 = \boxed{46.03 \text{ ft}^2}$$

$$A_s = \pi D L \rightarrow L = \frac{A}{\pi D} = \frac{4.27665}{\pi(0.01588)} = \boxed{85.7242 \text{ m}}$$

Since two tube pass length will be 42.8621 m

$$NTU = \frac{UA}{C_{min}} = \frac{(1250)(4.27665)}{3.486 \times 10^3} = \boxed{1.533}$$

From Fig 16-26 (c)

$$\epsilon = \boxed{65\%}$$

From Taco Catalogue given $A = 46.0334 \text{ ft}^2$

E8212L, 2 Pass, $A = 51 \text{ ft}^2$, 72 inches long

Chosen because it's in the middle of the 8" range and has a slightly larger area.

Better too buy! TACO heat exchanger is only 72 inches long.

Also most likely cheaper and less concerns about improper assembly.

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